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## 复合材料的动态响应

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### 引言

复合材料的动态响应, 从 20 世纪 60 年代中期以来, 一直是人们所热衷从事的研究课题。它是一个具有广泛技术应用的课题, 对理论和实验研究也提出了许多挑战性的问题。关于这个课题, 现在已有大批文献。人们提出了各种预计复合材料动态响应的理论。这个领域研究的最终目标是得出一种近似理论, 它相当简单, 同时又能相当精确地预计复合材料结构在承受动载荷时的响应。

尽管发表了大量研究论文, 这个目标似乎还没达到。这并不是反映了在该领域中缺乏研究能力。恰恰相反, 有几种成熟的理论能够精确地预计复合材料动态响应的某几方面的问题。这倒是反映了分析复合材料的困难。有人可能得出一种精确的或近于精确的理论, 但它不是在数学上难于处理, 就是在实践上难以做到。另一方面, 有人可能得出一种非常简单的近似理论, 但它过于粗糙, 甚至不能预示最简单的复合材料动态响应。

本文的目的是对现有预计复合材料动态响应的各种理论作一综述。它以评述文[1]中报告的主题作为出发点,该文包括了已发表的300多篇参考文献。关于复合材料动力学已公开发表的工作的另一些参考文献,可在[2—5]中找到。

### 近似理论

在这一节中,我们对现有的复合材料动态响应理论作一简略综述和比较。一种理论的有效性和适用性,决定于人们所要求的解的性质。一种理论可能对求解波传播的某几方面问题颇为有效,但是对求解波动现象的其他方面问题则是全然不合适的。在大多数情况下,一种理论的适用性反映了该理论中所做的假定。把各种理论的有效性作一比较,人们会提出下面一些问题:近似到什么程度以及怎样才容易计入高阶项以得到较好的近似?该理论是否易于用来求解瞬态问题?该理论是否适用于非线性复合材料和非线性复合材料?

对于一种给定的理论,人们不应期望对上述所有问题都有肯定的回答。否定的回答并不必然意味着该理论是低劣的。每一种理论有其长处和缺陷。理论的价值在于人们能用它解决实际问题。

**等效模量理论** Postma[6]和 White and Angona [7]<sup>1)</sup>提出的等效模量理论,将复合材料模拟为通常是各向异性的均匀介质,其材料常数是各种成分性能的几何加权平均值。宏观应力和应变之间的关系,通常只是在静态加载基础上得到的。在等效模量理论中,复合材料中的波速与频率无关。

尽管对静载荷下的一些几何结构得出了一些满意的结果,但是当应用于波的传播问题时,对于实际的所有几何结构来说,等效模量理论表现出严重的不足。特别是这些理

论不能反映出在复合材料中所观察到的色散和衰减。在主要信号的波长与复合材料典型微观尺度同量级时,色散和衰减效应变为重要。由于色散和衰减是与不连续材料性能有关的微结构所引起的,所以任何连续体理论无论如何必须考虑微观结构的影响。下述一些理论就是注意了这一意图而建立的。

应当提到,等效模量理论已应用于非线性和非弹性复合材料。根据上述理由,用这种理论能否正确地预示非线性或非弹性复合材料的动态响应,是有疑问的。

**等效刚度理论** 等效刚度理论是叠层介质和纤维增强复合材料的第一个近似连续体模型,它说明几何色散的典型动态效应,并从而反映复合材料微观结构的影响。此理论是在 Achenbach, Herrmann and Sun 的一系列论文[8—10]中发展起来的。这种理论的高阶理论是由 Turhan [11] 及 Drumhelle<sup>r</sup> and Bedford [12—14] 导出的。

等效刚度理论中有两个决定性步骤。我们以双层复合材料为例。首先,在每一层内的位移表达为该层的中面位移的 Taylor 级数(或其他多项式)。因此级数的系数只在一些离散的中面处定义。在层的界面处由位移的连续性得到了一个有限差分方程。在每层中,借助于假设的位移场,得到了应变、应变能和动能。第二个重要步骤是光滑化运算,运算中,先前仅在一些离散的位置处定义的函数被扩充而对所有的点定义。这可由取各层中应变能的加权平均来完成。假定层的厚度很小,连续性条件便可重写成微分形式。最后应用 Hamilton 原理,对所假设的位移场导出了最佳近似解。这就得到了关于复合材料中位移的微分方程组。

Sun, Achenbach and Herrmann [8]用这些位移方程研究在叠层介质中平面谐波的

<sup>1)</sup> 当然,在把等效模量理论用于复合材料的“静态”响应方面,有大量的工作。

传播。提出了谐波平行和垂直于铺层方向传播的色散关系,并把这种近似的色散曲线和 Rytov [15]得到的精确曲线作了比较。在波数趋于零时的极限相速度与精确极限一致。波在铺层方向传播的最低反对称模式示出了最强的色散,这一点,在一个相当宽的波数范围内由该理论非常恰当地描述出来。

等效刚度理论的精确性依赖于层中位移的级数展开,而这又取决于层的厚度。可以得到更高阶的近似,但人们不得不从出发点开始进行全部推导。此理论应用于瞬时问题时涉及求解微分方程的问题,其中最低阶的近似就有12个微分方程。

等效刚度理论已被用于有限变形[16]和粘弹性复合材料[17]。

混合体理论 由 Lempriere[18]提出的另一种方法是用混合体理论作为复合材料的动力学模型。连续体混合的基本概念是 Truesdell and Toupin[19]所主张的。Green and Naghdi [20,21], Steel [22], Tiersten and Jahanmir [23] 以及 McNiven and Mengi [24,25]作了进一步发展。在这些理论中,把结构上的复合材料的组分在空间进行叠加,并允许经受各别的变形。然后,通过确定组分相互作用的性质和混合体本构关系的形式来模拟复合材料的微观结构。

尽管控制混合体的一般守恒定律可以容易用公式表达出来,但实际应用于复合材料时却遇到了困难,其中,基于对各个组分的几何关系和本构关系的了解,用解析的方法确定组分间的相互作用是颇为困难的。Bedford and Stern[26]首先提出一种关于叠层复合材料的混合体理论,材料中的相互作用参数是根据某些简单的准静态问题的结果确定的。因此,在 Bedford and Stern [27—29] 以及 Hegemier, Gurtman and Nayfeh [30]的一系列论文中,对一些叠层的和纤维增强的复合材料的混合体理论取得

了不同程度的成功。

在混合体理论中,假定各组分是共存的,并允许有各自独立的运动,尽管已知各组分间是完全结合在一起的。关于各组分相对运动的假定,是这些理论的关键,也是改进这些理论的精确度的主要难关。虽然对简单的双层复合材料中的谐波已得出满意的结果,但假定其他复合材料各组分间有适当的相互作用的问题却依然存在。

混合体理论可用于谐波和瞬时波。有可能把它们推广到非线性复合材料上去,不过在确定各组分间的相互作用方面仍有着困难。

有相互作用的连续体理论 对于叠层复合材料和直接增强纤维复合材料,在根据渐近展开方法建立连续体模型上取得了相当大的成功。渐近展开中假定结构的特征长度与波长之比远小于1。Ben-Amoz[31,32]提出过一种利用直接渐近展开的方法,它适合于波导类型的问题。另一种方法是利用空间展开和渐近展开,是由 Hegemier 提出,并由 Hegemier and Nayfeh [33] Hegemier, Gurtman and Nayfeh [30] 及 Hegemier and Bache [34,35] 在一系列文章中发展了的。Hegemier 称他的理论为“有相互作用的连续体理论”。

我们再来考虑一下双层复合材料的例子。在有相互作用的连续体理论中,在每层的中面附近,不仅位移,而且应力也以空间变量的幂级数的形式展开。这里不是用 Hamilton 原理去求得该幂级数系数的近似微分方程,而是把位移和应力的整个幂级数代入运动方程和本构方程,得到幂级数系数的微分-递归关系。因此,应力和位移中较高阶的系数用最低阶系数来表达。原来的幂级数展开式则重新写成最低阶展开式系数对时间微分的级数。利用层与层交界面上应力和位移的连续性,得出双层复合材料中面处应

力和位移的四个微分差分方程。小厚度假定允许把该差分方程展开为 Taylor 级数, 并得到如下的偏微分方程:

$$\{\cosh(2r^{(1)}\epsilon\partial_\tau)\cosh(2r^{(2)}\epsilon\partial_\tau) + (20 - 1)\sinh(2r^{(1)}\epsilon\partial_\tau) \cdot \sinh(2r^{(2)}\epsilon\partial_\tau) - \cosh(2\epsilon\partial_\xi)\}\Phi = 0 \quad (1)$$

这里,  $\Phi$  可以是应力, 也可以是位移,  $\xi$  和  $\tau$  分别是无量纲坐标和时间。 $r$  和  $\theta$  取决于该弹性双层复合材料的几何结构和材料性质。上角(1)和(2)表示双层复合材料的各组分, 而  $\epsilon$  是个参数, 它是一个格子单元的厚度与某宏观特征尺寸的比值。

把方程(1)改写成

$$\{\theta\cosh(2r\epsilon\partial_\tau) - (\theta - 1)\cosh(2\delta\epsilon\partial_\tau) - \cosh(2\epsilon\partial_\xi)\}\Phi = 0 \quad (2)$$

这里,  $r = r^{(1)} + r^{(2)}$   
 $\delta = r^{(1)} - r^{(2)} \quad (3)$

对于小参数  $\epsilon$ , 可把方程(2)展开为

$$\{(1 + a_2\epsilon^2\partial_\xi^2 + a_4\epsilon^4\partial_\xi^4 + \dots)\partial_\xi^4 - (1 + b_2\epsilon^2\partial_\xi^2 + b_4\epsilon^4\partial_\xi^4 + \dots)\partial_\xi^2\}\Phi = 0 \quad (4)$$

这里, 由方程(2)可以容易地得到系数  $a_n, b_n$  ( $n=2, 4, 6, \dots$ ) 的显式[1]。令  $\epsilon = 0$ , 得到零阶近似, 这是由等效模量理论预言的。一阶理论(是  $\epsilon^2$  的一阶, 本来应称为二阶)得到比一阶等效刚度理论要好一些的结果。这并不奇怪, 因为一阶( $\epsilon^2$ )理论考虑了在层与层的交界面上位移和应力的连续性, 而等效刚度理论的一阶理论则只考虑了位移的连续性。可以建立一个与有相互作用的连续体一阶理论相当的二阶等效刚度理论[12]。

有相互作用的连续体理论具有很多有用的特征。首先, 由于包括高阶项而较容易地改进精确度。尤其是对于双层复合材料来说, 用方程(4), 我们可以得到一个封闭形式的显表达式, 它具有我们所要求的任意阶精度。其次, 这个理论可以用于复合材料的稳态振动, 也可用于复合材料的瞬态响应。

第三, 至少对双层复合材料来说由方程(1)或(2)可以容易地回到精确的频率方程。

然而, 这种理论不是没有缺点的。虽然方程(4)提供了高阶理论, 但时高阶微分方程来说, 满足初始条件和边界条件方面的困难限制了理论本身的应用。

没有理由认为这种理论不能推广到非线性复合材料中去。不过, 要是尝试建立比一阶再高的高阶理论的话, 它当然就变得不广泛了。

其他理论 有一些别的理论, 它们不象上述那些理论那样得到广泛的使用或公认。

在纤维增强复合材料中, 对在纤维方向上传播的波, 纤维起着波导的作用。对于在垂直于纤维方向传播的波, 纤维很少变形, 实际上它们好象是一些障碍物, 它们的行为与晶格组织中的质点类似, 阻碍着纤维之间以及纤维与周围介质之间的相互作用。这就引出了 Drumheller and Sutherland [36] 和 Nayfeh [37] 所考虑的关于复合材料的晶格模型。

在一系列论文中, Tsou and Chou [38, 39], Torvik [40], Chou and Wang [41], Munson and Schuler [42] 以及 Wang [43] 使用了一种控制体积法, 来计算纤维增强的和叠层的复合材料中冲击波运动的 Hugoniot 曲线。用这种方法, 他们不仅能确定平均 Hugoniot 曲线, 而且还能确定整个冲击波宽度范围内的界面剪应力的积分。

Eringen [44] 和 Habip [45] 研究出一种微观同构连续统理论。这种理论企图预计粒状固体, 各向异性体及聚合物流体, 尤其是复合材料的热力学性能和力学性能。在此理论中, 把力学场考虑为分布状态的。推导出控制场的任意阶矩的偏微分方程。还运用光滑化运算, 把所有各个组分的总和用一些在材料体积范围内的积分式来近似表示。

与位错的连续体理论中的微分几何方法

有关的邻域概念,是由 Ben-Amoz [46] 提出来的。他利用邻域平衡技术,回避了涉及材料不连续性的困难。然而组分的位移与相应的邻域平均之间的关系,必须以实验为前提和/或由实验推断。

Chao and Lee [47] 提出一种用于周期层状复合材料的离散连续体理论。其处理方法或多或少沿用了 [9] 的方法,不过没有光滑化处理。在此理论中,由推导出一个二项截断 Taylor 级数,得到了每一层的位移场。结合交界面连续性条件的控制方程是以微分差分方程组的形式推导出来的。

实验中观察到的在弹性复合材料中波的衰减,促使 Barker [48] 把弹性复合材料模拟为均匀的粘弹性材料。他假定了一种 Maxwell 型粘弹性材料,并且合理地预示了复合材料的总体瞬态响应。弹性复合材料和均匀粘弹性介质之间的相似性,也曾由 Chen and Gurtin [49] 在他们的加速度波研究中指出过。在这些研究结果的鼓舞下,Christensen 进一步追随这种思想,并指出粘弹性模型的松弛函数必须是时间的振荡函数 [50]。为了求解层状复合材料中瞬态波的传播,最近 Ting and Mukunoki [51,52] 把粘弹性比拟的思想更精确地用公式表达出来。下面我们将再谈到这点。

#### 应用

在这一节中,我们将讨论一下上述近似理论的某些应用,同时也讨论一下我们没有叙述过的但是是用于解决复合材料动态响应某些特定问题的那些理论的应用。

谐波 对于大多数近似理论,理论正确性的第一个验证,是应用该理论去求出由谐振得来的复合材料的频率方程,并且在有精确解时,与之比较其结果。然而,如果得出的频率方程是与人们所期望的一样,那么,当没有精确的频率方程时,就可以用其他的数学近似方法求出频率方程。

Kohn, Krumhansl and Lee [53] 使用根据 Floquet 或 Bloch 理论建立的变分法,研究了弹性谐波通过只有周期结构的复合材料的传播。把 Rayleigh-Ritz 方法应用于变分方程的解以计算色散关系、相速度和应力波形。在另一篇文章中, Lee and Yang [54] 把这种解与简正模理论的解作了比较。

Nemat-Nasser 和他的同事们在一系列论文中 [55—58], 把比在 [53] 中所考虑过的更为一般的变分原理用于 Floquet 波问题。在 Hellinger-Reissner 变分法的基础上,他发展了广义变分原理,其中,在一种情况下以位移、应力和应变作为给定的自变量。在另一种状况下以位移和应力作为给定的自变量。根据这种广义变分原理,他推导出了与 Rayleigh 比商不同的新比商,以确定复合材料中的谐波频率。数值分析的例子表明,这些解非常迅速地收敛于精确解。

文献中考虑过的复合材料中的大多数谐波,是对于无限大的复合材料而言的。Herrmann et al. [59] 研究了在有限大层状介质中水平偏振的剪切谐波。同样,在频率方程研究方面,大多数只考虑波数为实数的情况。Delph, Herrmann and Kaul [60,61] 给出了注意到有复波数和注意到 Brillouin 区域末端的层状介质的频率方程的详细研究。

瞬态波 对线弹性复合材料来说,一旦复合材料的频率方程已知,复合材料中瞬态波的传播就可以由 Fourier 综合法 [62] 得到。然而在实践中,除了对于只适用于时间很长时的渐近解 [63—66] 之外,几乎很少的解是用这种方法求得的,对于时间为有限时的解,可以用高阶渐近展开 [67]。然而,渐近解并不十分实用,特别是当复合材料是有限尺寸的以及边界条件是和时间相关的时候。

由 Barker [48] 首创的把弹性复合材料模拟成均匀粘弹性介质的思想,被发展来确定在有限时间内的瞬态响应。问题的关键是

找到这种“等效的”粘弹性材料的松弛函数。基于介电理论, Christensen[50]指出, 这种等效粘弹性材料的松弛函数是时间的振荡函数。最近, Ting and Mukunoki [51]对垂直于铺层方向传播的波的情况, 导出了松弛函数的精确形式。于是通过求解等效的均匀粘弹性材料中的瞬态波, 可得出弹性复合材料中的瞬态波。一个有关弹性双层复合材料的数值例子表明, 由这种粘弹性比拟理论得到的解, 与由射线理论得到的精确解非常符合。粘弹性比拟理论应用到叠层复合材料时, 叠层复合材料的每一成分可以是弹性的, 也可以是粘弹性的。这种比拟也可应用于有限尺寸的层状复合材料[52]。

**非线性波** 在复合材料中非线性波的传播, 是一个分析起来比线性波传播困难得多的问题。实际上不可能得到精确解, 除非是极简单的情况, 例如曾由 Chen and Gurtin [49]考虑过的情况, 加速度波在非线性波中, 从光滑变化的初始条件产生冲击波是一件合乎规律的事情而不是一个例外。因此, 任何解复合材料中非线性波传播问题的尝试, 完全或几乎完全不会成功。

一些非线性问题已用近似方法求解。叠层复合材料的大变形由 Grot and Archenbach [16] 考虑过。用二阶非线性几何声学理论, Seymour and Mortell [68] 研究了在叠层复合材料中反射对非线性瞬态脉冲的影响。Sun et al. [69] 考虑了非线性弹性纤维增强复合材料。至于弹塑性复合材料, 它们当然是非线性的, 已由 Hegemier [70], Hegemier and Gurtman [71] 及 Ben-Amoz [72] 研究过。

**复合材料结构** 仅次于复合材料中的谐波问题, 复合材料做成的结构零件的动态响应可能是最广泛被研究的课题。这是由于它有着直接的工业应用。关于这个课题, 我们仅能列举少量已公开发表的工作。

纤维增强复合材料杆的问题由 Tauchert and Moon [73] 考虑过。对于复合材料弹性圆柱体, Lai et al. [74] 研究过谐波的传播, Haines et al. [75] 考察过扭转波。Armenakas [76,77] 研究了谐波在复合材料圆柱壳中的传播, 他也研究过叠层梁[78]。三层梁的非线性振动由 Hyer et al. [79] 研究过。

对复合材料的平板和球壳, 曾考虑过许多问题。Sun[80]提出一种复合材料平板的精细的理论。关于复合材料平板方面考虑过的其他问题有谐振[81—83], 非线性振动[84, 85], 波的传播[86—88], 弯曲波[89,90], 波面[91], 以及屈曲[92]。关于球壳, [93—95] 研究了谐振, 而[96]考虑了波传播问题。

我们再次强调, 这里所说的参考资料仅仅是一些例子, 还远远不全。

### 结论

当然, 这里列举的一些理论和方法, 仅仅是分析复合材料动态响应的许多方法中的几个。另一些方法, 象实验和数值方法, 在这里没有包括。即使在理论分析范围内, 我们还没有论及的一些课题有: 稍作增强的复合材料[97], 随机增强的复合材料[98—100], 纤维方向不断变化的复合材料[101], 纤维使波散射的复合材料[102,103], 周期不太规则的层状复合材料[104], 等等。这个目录还可以再开列下去。对复合材料动态响应方面研究的热潮, 在20世纪70年代初期达到高峰之后, 看来有点减退。为什么呢? 这并不是因为没有更多的问题需要解决。而是因为较容易的一些问题已经解决了, 而留下的是一些难题。

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